

# UM10411

120 Watt notebook adapter with TEA1752T and TEA1791T

Rev. 1 — 19 October 2010

User manual

## Document information

Info	Content
<b>Keywords</b>	GreenChip-III, TEA1752T, GreenChip-SR, TEA1791T, PFC, flyback, synchronous rectification, high efficiency, adapter, notebook, PC power
<b>Abstract</b>	This manual provides the specification, performance, schematics, bill of materials and PCB layout of a 120 W notebook adapter using the TEA1752T and TEA1791T.



**Revision history**

Rev	Date	Description
v.1	20101019	First issue

**Contact information**

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## 1. Introduction

### WARNING

#### Lethal voltage and fire ignition hazard



The non-insulated high voltages that are present when operating this product, constitute a risk of electric shock, personal injury, death and/or ignition of fire.

This product is intended for evaluation purposes only. It shall be operated in a designated test area by personnel qualified according to local requirements and labor laws to work with non-insulated mains voltages and high-voltage circuits. This product shall never be operated unattended.

This manual describes a universal input, 19.5 V, 6.15 A single output power supply using TEA1752T and TEA1791T devices from the GreenChip-III and GreenChip Synchronous Rectification (SR) family of NXP Semiconductors. It contains the specification of the power supply, circuit diagram, the component list to build the supply, the PCB layout and component positions and documentation of the Power Factor Correction (PFC) choke and transformer, as well as test data and oscilloscope graphs of the most important waveforms. For design details on the TEA1752T and TEA1791T refer to the application note.

The GreenChip-III combines the control and drive for both the PFC and the flyback stages into a single device. The TEA1752T provides complete Switched Mode Power Supply (SMPS) control functionality in compliance with IEC61000-3-2 harmonic current emission requirements, a significant reduction of components, saving PCB space and providing a cost benefit. It also offers extremely low power consumption in no-load mode which makes it suitable for the low power consumer markets. The built-in green functions ensure high efficiency at all power levels, which results in a design that can easily meet all existing and proposed energy efficiency standards such as: European Union Code of Conduct (CoC), ENERGY STAR (US), California Energy Commission (CEC), Minimum Performance Energy Standards (MEPS) (Australian and New Zealand) and China Energy Conservation Program (CECP).

The GreenChip-SR is a synchronous rectification control IC that needs no external components to tune the timing. Used in notebook adapter designs, the GreenChip-SR offers a wide  $V_{CC}$  operating range between 8.5 V and 38 V, minimizing the number of external components required and enabling simpler designs. In addition, the high driver output voltage (10 V) makes the GreenChip-SR compatible with all brands of MOSFETs.



001aa826

Fig 1. 120 W TEA1752T and TEA1791T demo board

## 2. Specification

- Mains input voltage: 90 V to 264 V; 47 Hz to 63 Hz
- DC output: 19.5 V;  $\pm 2\%$
- Maximum continuous output current: 6.15 A
- Peak output current:  $\geq 7.6$  A
- Efficiency:  $\geq 87\%$  at maximum load
- ENERGY STAR active mode efficiency:  $> 89.5\%$
- No load power consumption:  $\leq 0.25$  W
- Dynamic load response (peak-to-peak): 700 mV
- Output ripple and noise (peak-to-peak): 100 mV
- CISPR22 class B conducted ElectroMagnetic Interference (EMI) (Pass)
- EN61000-4-2 immunity against ElectroStatic Discharge (ESD) ( $\geq 12$  kV air discharge)
- EN61000-3-2 A14 (harmonics) compliance
- Short-circuit Protection (SCP); input power  $< 1.2$  W during SCP test
- OverCurrent Protection (OCP); input power  $< 2.2$  W during OCP test
- Latched output OverVoltage Protection (OVP):  $< 24$  V
- Latched OverTemperature Protection (OTP);  $\leq 120$  °C
- Fast Latch Reset (FLR):  $< 2$  s

### 3. Performance data

#### 3.1 Test setup

##### 3.1.1 Test equipment

- AC source: Agilent 6812B
- Power meter: Yokogawa WT210 with harmonics option
- DC electronic load: Chroma, Model 63103
- Digital oscilloscope: Yokogawa DL1640L
- Current probe Yokogawa 701933 30A; 50 MHz
- 100 MHz, high voltage differential probe: Yokogawa 700924
- 500 MHz, low voltage differential probe: Yokogawa 701920
- Multimeter: Keithley 2000
- ElectroMagnetic Compatibility (EMC) receiver: Rohde and Schwarz ESPI-3 + Line Impedance Standardization Network (LISN) ENV216

##### 3.1.2 Test conditions

- Adapter on the lab-table with heat sinks facing downwards
- The adapter has no casing
- Ambient temperature between 20 °C and 25 °C
- Measurements were made after stabilization of temperature according to "test method for calculating the efficiency of single-voltage external AC-to-DC and AC-to-AC power supplies" of ENERGY STAR

#### 3.2 Efficiency

##### 3.2.1 ENERGY STAR efficiency

To market adapters as ENERGY STAR efficient they must pass the active mode and no-load criteria as stated in the ENERGY STAR standard for External Power Supplies; EPS2.0. The minimum active-mode efficiency is defined as the arithmetic average efficiency at 25 %, 50 %, 75 % and 100 % of the rated output power as printed on the nameplate of the adapter.

###### 3.2.1.1 Active mode efficiency

###### Test conditions:

The adapter is set to maximum load and preheated until temperature stabilization is achieved. Temperature stabilization is established for every load step before recording any measurements.

**Remark:** The output voltage is measured at the end of the output cable ( $2 \times 20 \text{ m}\Omega$ ).

**Pass criteria:**

To comply with ENERGY STAR EPS2.0, the arithmetic average of the four efficiency measurements must be  $\geq 87\%$ . Universal mains adapters must pass the criteria at both 115 V; 60 Hz and 230 V; 50 Hz. To meet this criteria, the PFC must be off at 25 % load and preferably on at 50 % load.

**Table 1. Active mode efficiency at 115 V; 60 Hz**

Load (%)	I <sub>O</sub> (A)	V <sub>O</sub> (V)	P <sub>O</sub> (W)	P <sub>I</sub> (W)	Efficiency (%)	Power factor
100	6.163	19.115	117.81	132.96	88.6	0.984
75	4.616	19.217	88.70	98.57	90.0	0.974
50	3.083	19.318	59.55	65.72	90.6	0.952
25	1.538	19.407	29.85	32.77	91.1	0.461
Average	-	-	-	-	90.0	-

**Table 2. Active mode efficiency at 230 V; 50 Hz**

Load (%)	I <sub>O</sub> (A)	V <sub>O</sub> (V)	P <sub>O</sub> (W)	P <sub>I</sub> (W)	Efficiency (%)	Power factor
100	6.163	19.108	117.77	131.56	89.5	0.935
75	4.616	19.210	88.67	98.74	89.8	0.903
50	3.083	19.313	59.54	67.14	88.7	0.843
25	1.538	19.413	29.86	32.79	91.1	0.381
Average	-	-	-	-	89.8	-

**Table 3. PFC on and off level as a function of mains input voltage**

Mains supply	90 V; 60 Hz	100 V; 50 Hz	115 V; 60 Hz	230 V; 50 Hz	264 V; 50 Hz
Output current (A) (PFC on)	2.21	2.28	2.51	2.58	2.57
Output current (A) (PFC off)	1.81	1.82	1.85	1.84	1.78

**3.2.1.2 No-load input power****Test conditions:**

The adapter is set to maximum load and preheated. After five minutes the load is removed. The no-load input power measurements were recorded after stabilization of the input power reading.

**Pass criteria:**

To comply with ENERGY STAR EPS2.0, the input power must be less than 0.5 W. Universal mains adapters must pass the criteria at both 115 V; 60 Hz and 230 V; 50 Hz.

The adapter is set to maximum load and preheated. After five minutes the load is removed. The no-load input power measurements were recorded after stabilization of the input power reading.

**Table 4. No-load input power***No-load input power as a function of the mains input voltage.*

Mains supply	90 V; 60 Hz	100 V; 50 Hz	115 V; 60 Hz	230 V; 50 Hz	264 V; 50 Hz
Input power P <sub>I</sub> (W)	0.135	0.139	0.143	0.210	0.240

### 3.2.1.3 Full load efficiency PFC plus flyback stage

#### Test conditions:

Before any measurements were recorded, the adapter is set to maximum load and is preheated until the readings were stabilized.

**Remark:** The output voltage is measured at the end of the output cable. ( $2 \times 20 \text{ m}\Omega$ )

#### Pass criteria:

The efficiency ( $\eta$ ) must be  $\geq 87\%$  at the maximum continuous output load.

**Table 5. PFC plus flyback stage***Total converter efficiency (at full load) as a function of the mains input*

Mains supply	I <sub>I</sub> RMS (A)	P <sub>O</sub> (W)	P <sub>I</sub> (W)	Efficiency (%)	Power factor
(V)	(Hz)				
90	60	1.52	117.71	135.07	87.1
100	50	1.35	117.78	134.09	87.8
115	60	1.17	117.81	132.96	88.6
230	50	0.61	117.77	131.56	89.5
264	50	0.54	117.81	131.36	89.7

## 3.3 Timing and protection

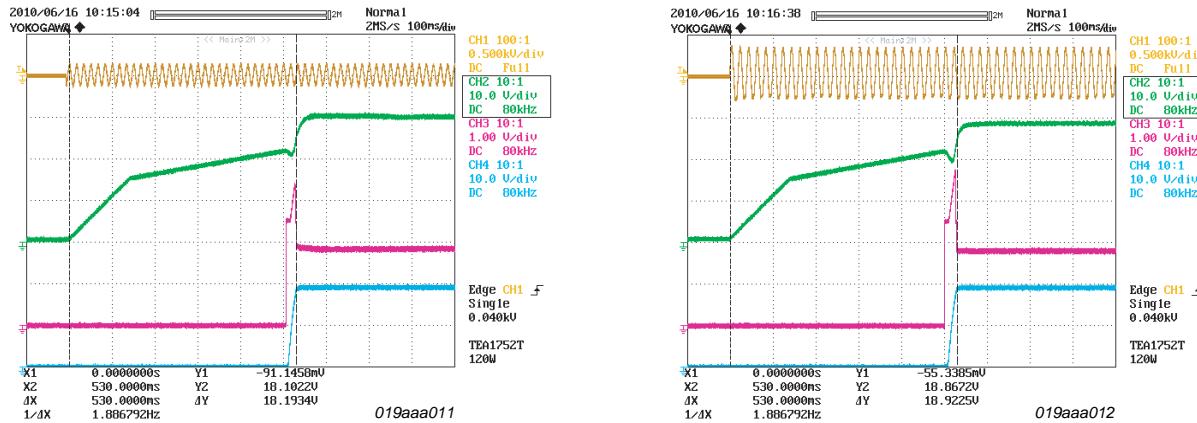
### 3.3.1 Switch-on delay and output rise time

#### Test conditions:

The electronic load is set to Constant Current (CC) mode and  $V_{on} = 0 \text{ V}$ . The electronic load is set to the maximum continuous output current.

#### Pass criteria:

- Switch-on delay: 2 seconds maximum from application of the AC mains voltage is applied to the time when the output is within regulation
- Output rise time: The output voltage must rise from 10 % of the maximum to the regulation limit within 30 ms. There must be a smooth and continuous ramp-up of the output voltage. No voltage with a negative polarity must be present at the output during start-up
- No output bounce or error is allowed during switch-on
- There must be sufficient margin between the FBCTRL signal and the 4.5 V time-out trigger level to avoid false triggering of the time-out protection due to component tolerances



a. Mains input 90 V; 60 Hz; delay time 484 ms

Load = 6.15 A

CH1: mains input

CH2: pin Vcc TEA1752T

CH3: pin FBCTRL TEA1752T

CH4: output voltage

b. Mains input 264 V; 50 Hz; delay time 484 ms

Load = 6.15 A

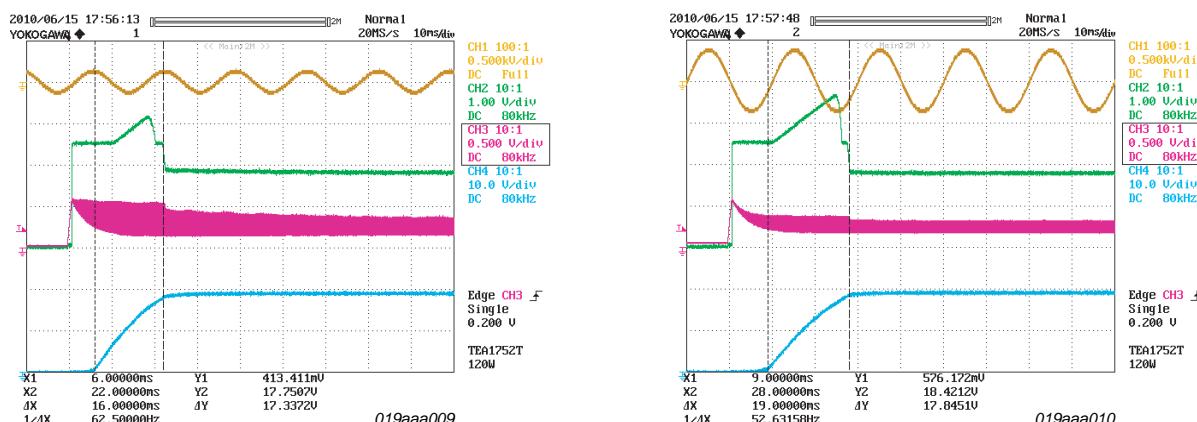
CH1: mains input

CH2: pin Vcc TEA1752T

CH3: pin FBCTRL TEA1752T

CH4: output voltage

Fig 2. Delay between switch-on and output in regulation



a. Mains input 90 V; 60 Hz; output rise time 12.64 ms

Load = 6.15 A

CH1: mains input

CH2: pin FBCTRL TEA1752T

CH3: pin FBSENSE TEA1752T (soft start)

CH4: output voltage

b. Mains input 264 V; 50 Hz; output rise time 12.24 ms

Load = 6.15 A

CH1: mains input

CH2: pin V<sub>CC</sub> TEA1751T

CH3: pin FBSENSE TEA1751T (soft start)

CH4: output voltage

Fig 3. Output rise time at full load start-up

### 3.3.2 Brownout and brownout recovery

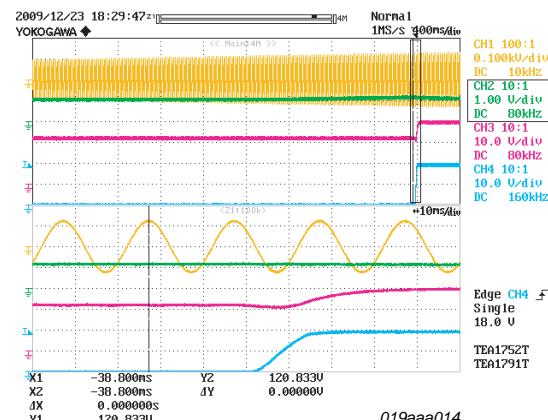
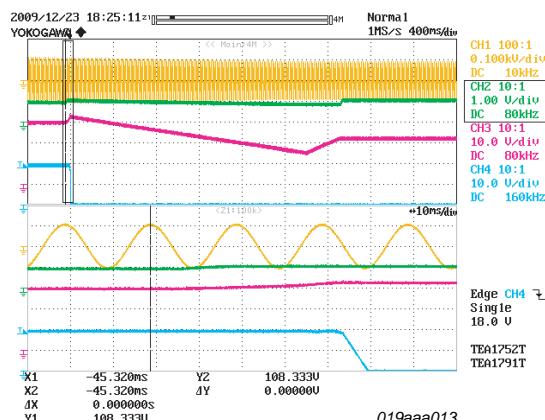
The voltage on pin VINSENSE is monitored continuously to prevent the PFC from operating at very low mains input voltages.

#### Test conditions:

The mains input voltage is decreased from 90 V to 0 V and then increased from 0 V to 90 V. The electronic load is set to CC mode and  $V_{on} = 0$  V. The electronic load is set to the maximum continuous output current.

#### Pass criteria:

- The adapter must survive the test without damage and excessive heating of component
- The output voltage must remain within the specified regulation limits or switch-off
- No output bounce or error is allowed during switch-on or switch-off
- The adapter must power-up before the AC line input voltage reaches 85 V (maximum)



a. AC mains input from 90 V to 0 V

$$\text{brownout voltage} = 108/(\sqrt{2}) = 76 \text{ V}$$

Load = 4.62 A

CH1: mains input

CH2: pin VINSENSE TEA1752T

CH3: pin  $V_{CC}$  TEA1752T

CH4: output voltage

b. AC mains input from 0 V to 90 V

$$\text{brownout recovery voltage} = 121/(\sqrt{2}) = 86 \text{ V}$$

Load = 4.62 A

CH1: mains input

CH2: pin VINSENSE TEA1752T

CH3: pin  $V_{CC}$  TEA1752T

CH4: output voltage

**Fig 4. Brownout and brownout recovery**

### 3.3.3 Output short-circuit protection

To protect the adapter and application against an output short-circuit or a single fault open (flyback) feedback loop situation, time-out protection is implemented. When the voltage on pin FBCTRL rises above 4.5 V, a fault is assumed and switching is blocked.

The time-out protection must not trigger during a normal start-up with the maximum continuous output current.

**Test conditions:**

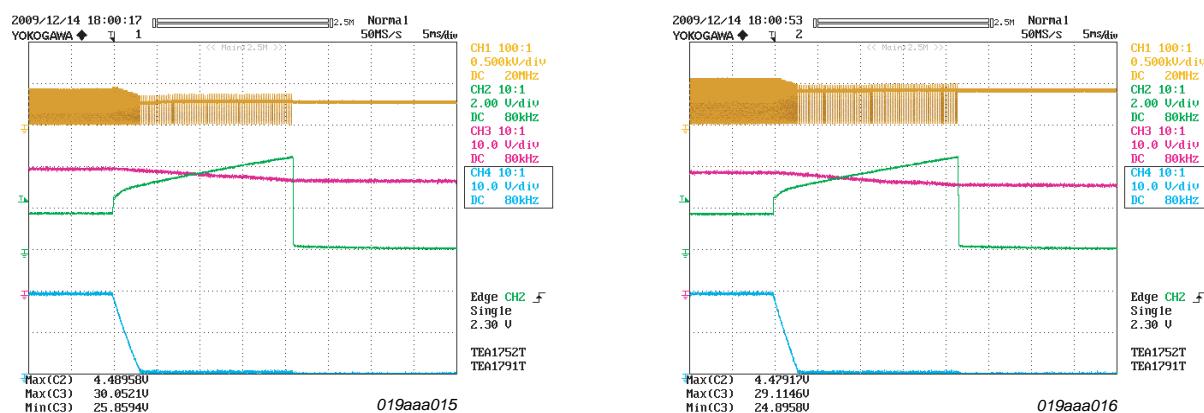
There are two test conditions:

1. The adapter is switched on with 6.15 A output load. After start-up a short-circuit is applied manually at the end of the output cable
2. Before the adapter is switched on a short-circuit is applied to the end of the output cable

**Remark:** An output short-circuit is defined as an output impedance of less than  $0.1 \Omega$ .

**Pass criteria:**

- The adapter must be capable of withstanding a continuous short-circuit at the output without damaging or overstressing the adapter under any input conditions
- The average input power must be less than 3 W during the short-circuit test
- The adapter must automatically recover after removal of the short-circuit



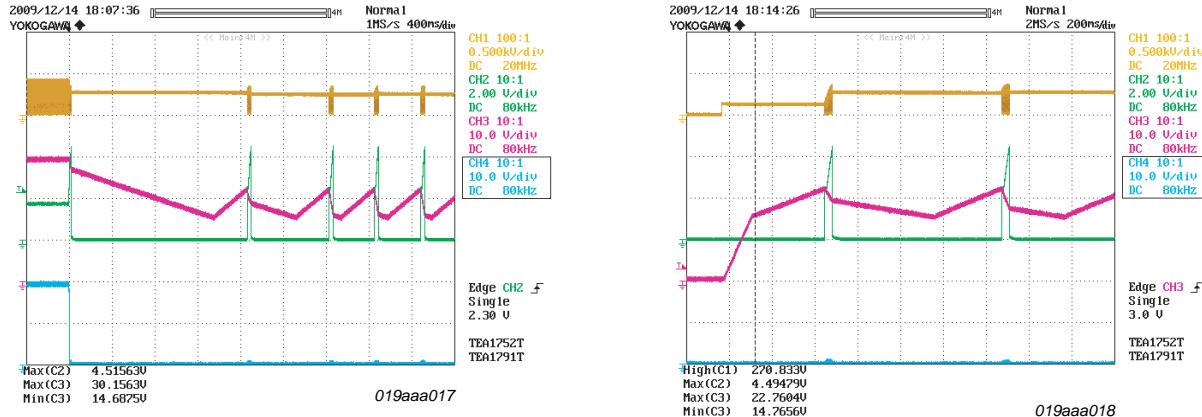
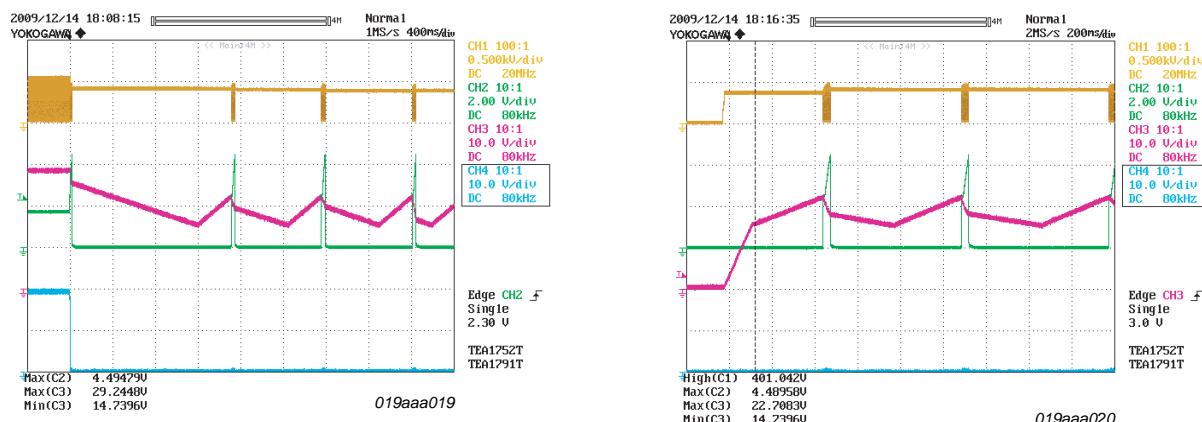
a. Mains input 90 V; 60 Hz

Load before short-circuit = 6.15 A  
CH1: drain flyback MOSFET  
CH2: pin FBCTRL TEA1752T  
CH3: pin  $V_{CC}$  TEA1752T  
CH4: output voltage

b. Mains input 264 V; 50 Hz

Load before short-circuit = 6.15 A  
CH1: drain flyback MOSFET  
CH2: pin FBCTRL TEA1752T  
CH3: pin FBDRIVER TEA1752T  
CH4: output voltage

**Fig 5. Output short-circuit, triggering of the time-out protection**

**Fig 6. Output short-circuit at 90 V; 60 Hz****Fig 7. Output short-circuit at 264 V; 50 Hz**

**Table 6. Output short-circuit input power***Output short-circuit input power as a function of the mains input voltage*

Mains supply	90 V; 60 Hz	100 V; 50 Hz	115 V; 60 Hz	230 V; 50 Hz	264 V; 50 Hz
Input power $P_1$ (W)	1.81	1.75	1.71	1.56	1.05

### 3.3.4 Output OverCurrent protection

**Test conditions:**

- The electronic load is set in CC mode
- The load is increased from the maximum continuous value in small steps until the OCP is triggered. The input power is measured after triggering over the OCP without changing the load setting

**Pass criteria:**

- The output power must be limited to less than 150 W, just before the triggering of the OCP
- The average input power must be less than 3 W once the OCP has been triggered

**Table 7. Output OCP and input power as a function of the mains input voltage**

Mains supply	90 V; 60 Hz	100 V; 50 Hz	115 V; 60 Hz	230 V; 50 Hz	264 V; 50 Hz
OCP (A)	7.9	7.9	7.9	7.5	7.5
Input power $P_1$ (W)	2.3	2.2	2.2	2.2	1.1

### 3.3.5 Output OverVoltage protection

**Test conditions:**

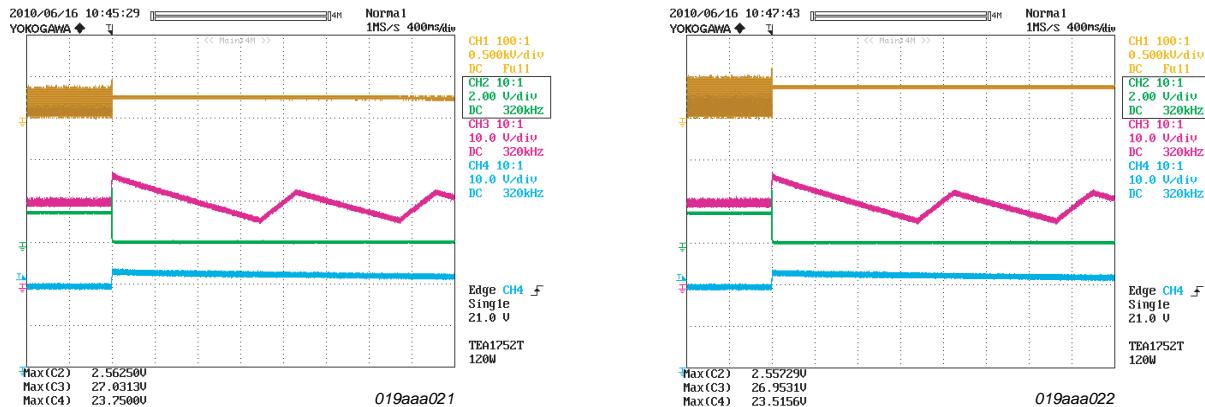
- The adapter is switched on without a load at the output
- An output over-voltage is created by applying a short-circuit across the opto LED of U2

**Pass criteria:**

- The output voltage must not exceed 25 V or stabilize between 25 V and the rated output voltage
- The voltage on TEA1752T pin  $V_{CC}$  must not exceed the absolute maximum rating of 38 V
- When OVP is triggered, the primary side controller must shutdown and stay in a latched mode
- A single point fault must not cause a sustained overvoltage condition at the output

**Table 8. Output OVP***Output over-voltage at no-load as a function of the mains input voltage with protection mode latched*

Mains supply	90 V; 60 Hz	100 V; 50 Hz	115 V; 60 Hz	230 V; 50 Hz	264 V; 50 Hz
Output OVP trip point (V)	23.4	23.4	23.2	23.3	23.3
$V_{CC}$ maximum during OVP (V)	27.2	27.2	27.1	27.0	27.0



- a. Mains input 90 V; 60 Hz

Load before short-circuit = 0 A  
 CH1: drain flyback MOSFET  
 CH2: pin FBCTRL TEA1752T  
 CH3: pin V<sub>CC</sub> TEA1752T  
 CH4: output voltage

- b. Mains input 264 V; 50 Hz

Load before short-circuit = 0 A  
 CH1: drain flyback MOSFET  
 CH2: pin FBCTRL TEA1752T  
 CH3: pin V<sub>CC</sub> TEA1752T  
 CH4: output voltage

Fig 8. Output OVP

### 3.3.6 OverTemperature protection

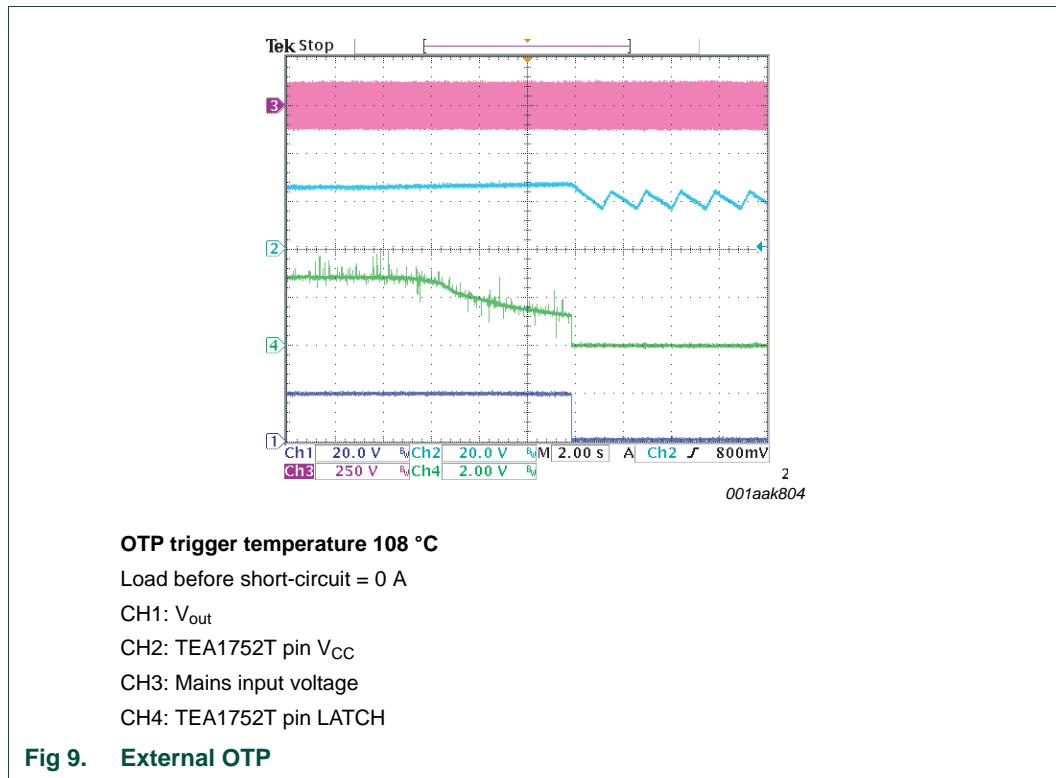
An accurate external OTP (TEA1752T pin LATCH, RT2, R26 and C19) is provided on the demo board to protect the flyback transformer against overheating (see [Figure 14](#)). Normally, the flyback transformer is the most heat sensitive component.

#### Test conditions:

The NTC temperature sensor glued to the transformer, is heated using a heat gun.

#### Pass criteria:

The IC must latch off the output at a VLATCH trip level of 1.25 V. No output bounce or error is allowed.



### 3.3.7 Fast latch reset

A FLR function enables latched protection to be reset without discharging the bulk elcap. The latch protection is reset as soon as the voltage on pin VINSENSE drops below 0.75 V and is then increased to 0.87 V.

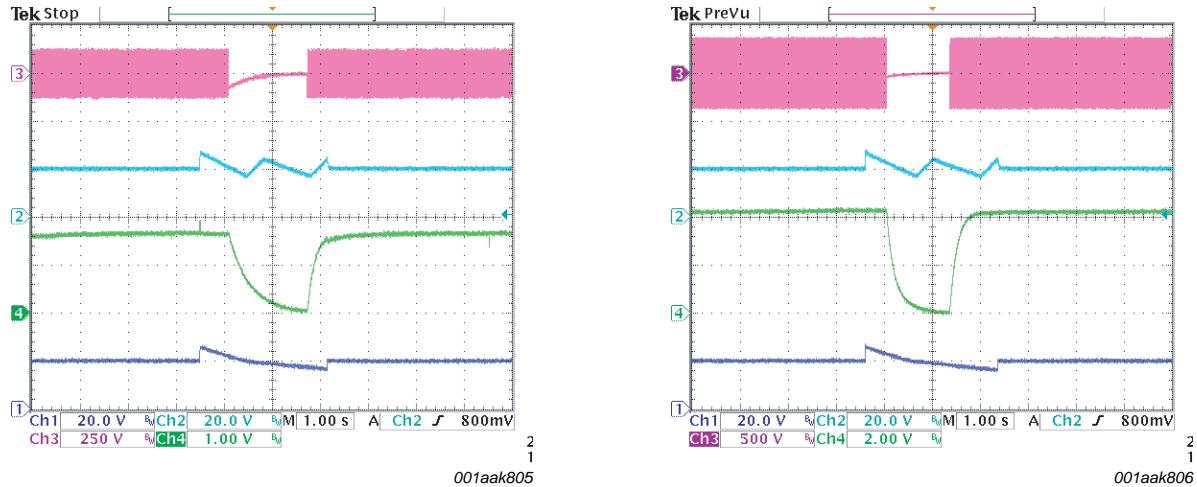
#### Test conditions:

- The output is not loaded
- The test sequence is as follows:
  - The latch protection is triggered by an OVP caused by a short-circuit across the OPTO LED
  - The mains input is switched off and the voltage on pin VINSENSE dropped below 0.75 V
  - The mains input is switched on and, as soon as the voltage on pin VINSENSE rises above 0.87 V, the latch is reset

**Remark:** Both live and neutral must be switched.

#### Pass criteria:

The latch must be reset within 3 seconds after switching off and switching on the mains input voltage.



a. Mains input 90 V; 60 Hz; FLR = 1.6 s

CH1: V<sub>out</sub>

CH2: pin V<sub>CC</sub> TEA1752T

### CH3: AC mains input

CH4: pin VINSENSE TEA1752T

b. Mains input 264 V; 50 Hz; FLR = 1.3 s

CH1: V<sub>out</sub>

CH2: pin V<sub>CC</sub> TEA1752T

### CH3: AC mains input

CH4: pin VINSENSE TEA1752T

### 3.4 Output regulation and characterization

### 3.4.1 Load regulation

#### **Test conditions:**

- The output voltage deviation is measured while the load current on the output is increased from 0 A to 6.15 A
  - The measurement is repeated for different mains input voltages

**Remark:** The output voltage is measured at the end of the output cable ( $2 \times 20 \text{ m}\Omega$ ).

### **Pass criteria:**

The output load regulation must remain within 2 %.

The load regulation is calculated using Equation 1.

$$\frac{V_{O(max)} - V_{O(min)}}{V_{O(nom)}} \times 100 \% \quad (1)$$

where  $V_{O(nom)} = 19.5$  V.

**Table 9** Load regulation

**Table 9. Load regulation**  
*Output voltage as a function of the output load and the mains input voltage*

Mains supply	90 V; 60 Hz	90 V; 60 Hz	264 V; 50 Hz	264 V; 50 Hz
$V_O$ ; $I_O$ (V; A)	19.160; 6.15	19.470; 0	19.165; 6.15	19.471; 0

Load regulation at 90 V; 60 Hz is calculated as follows:

$$\frac{19.470V - 19.160V}{19.5V} \times 100\% = 1.6\% \quad (2)$$

Load regulation at 264 V; 50 Hz is calculated as follows:

$$\frac{19.471V - 19.165V}{19.5V} \times 100\% = 1.6\% \quad (3)$$

### 3.4.2 Line regulation

**Test conditions:**

- The output voltage deviation is measured while the mains voltage on the input is increased from 90 V to 264 V
- The measurement is repeated for different mains input voltages

**Remark:** The output voltage is measured at the end of the output cable. The load current is 6.15 A.

The line regulation is calculated using the following equation:

$$\frac{V_{O(max)} - V_{O(min)}}{V_{O(nom)}} \times 100\% \quad (4)$$

**Pass criteria:**

The output voltage deviation must remain within 0.05 %.

**Table 10. Line regulation**

*Output voltage (at full load) as a function of the mains input voltage*

Mains supply	90 V; 60 Hz	100 V; 50 Hz	115 V; 60 Hz	230 V; 50 Hz	264 V; 50 Hz
V <sub>O</sub> (V)	19.147	19.147	19.147	19.148	19.148

Load regulation at 90 V; 60 Hz is calculated using the following equation:

$$\frac{19.148V - 19.147V}{19.5V} \times 100\% = 0.005\% \quad (5)$$

### 3.4.3 Ripple and noise periodic and random deviation

Ripple and noise are defined as the periodic or random signals over a frequency band of 10 Hz to 20 MHz.

**Test conditions:**

- The measurement is made with an oscilloscope set to a bandwidth of 20 MHz
- The output is shunted at the end of the output cable by a 0.1 µF ceramic disk capacitor and a 22 µF electrolytic capacitor to simulate loading

**Pass criteria:**

The output ripple and noise must remain within the specified limits 100 mV (peak-to-peak) at a maximum load current of 6.15 A.

**Table 11. Ripple and noise PARD***Ripple and noise (at maximum load) as a function of the mains input voltage.*

Mains supply	90 V; 60 Hz	100 V; 50 Hz	115 V; 60 Hz	230 V; 50 Hz	264 V; 50 Hz
PARD (mV)	86	86	86	75	75

### 3.4.4 Dynamic load response

**Test conditions:**

- The adapter is subjected to a load change from 0 % to 100 % at a slew rate of 1 A/ms
- The frequency of change is set to provide the best readability of the deviation and setting time

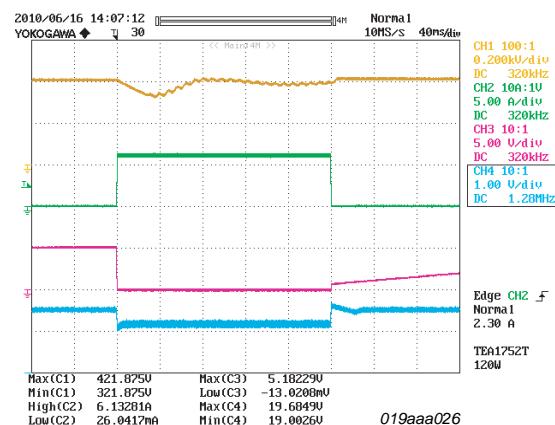
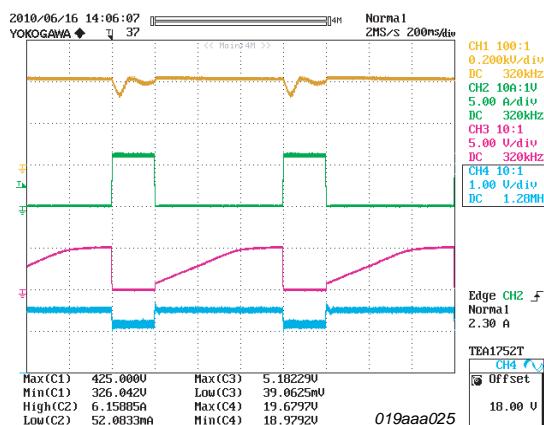
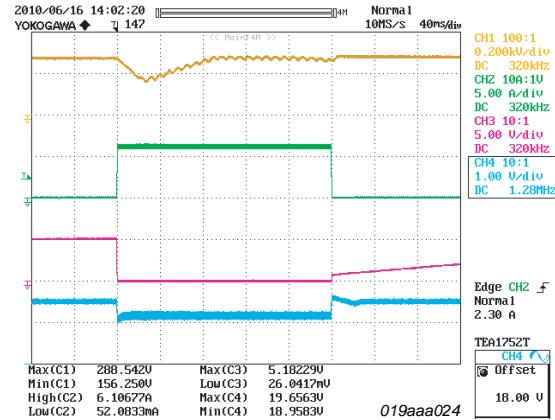
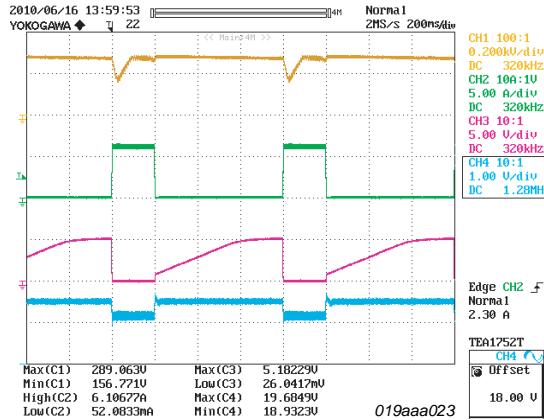
**Remark:** The voltage is measured at the end of the output cable.

**Pass criteria:**

The output must not overshoot or undershoot beyond the specified limits (+1 V to 0.5 V) after a load change.

**Table 12. Dynamic load response***Deviation of the output voltage at a load step from 6.15 A to 0 A and from 0 A to 6.15 A*

Mains supply	90 V; 60 Hz	100 V; 50 Hz	115 V; 60 Hz	230 V; 50 Hz	264 V; 50 Hz
Deviation (mV <sub>p-p</sub> )	700	700	700	700	700

**Fig 11. Dynamic load response**

## 4. ElectroMagnetic compatibility

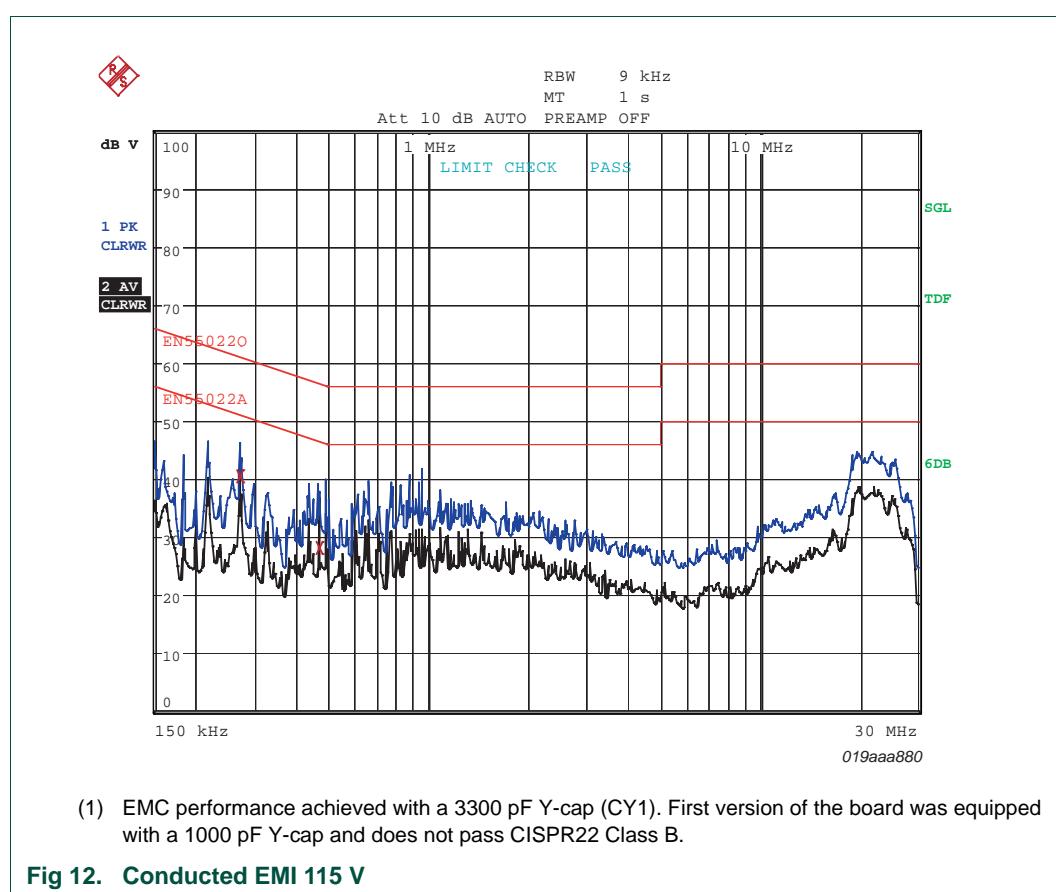
### 4.1 Conducted emission

#### Test conditions:

- The adapter is subjected to maximum load
- The ground connection of the output cable is connected to EMC ground

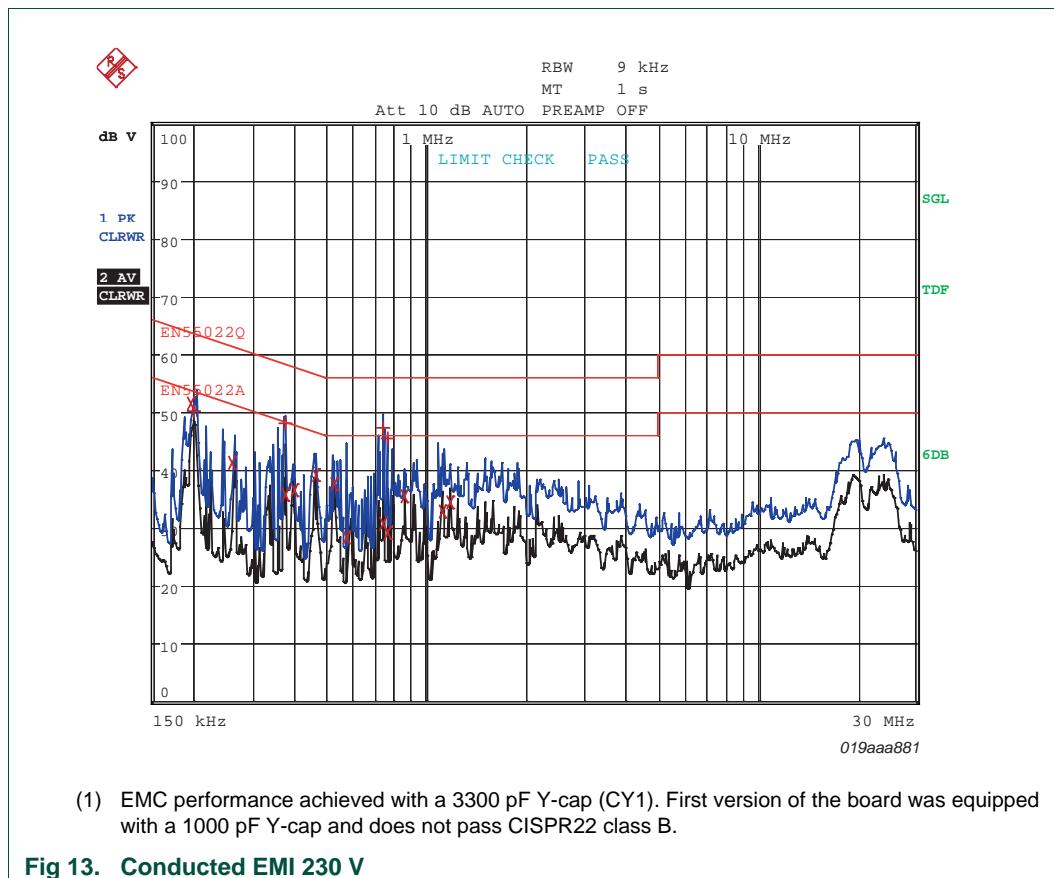
#### Pass criteria:

CISPR22 Class B



**Table 13. Conducted EMI measurement 115 V**

Frequency (MHz)	Phase	Detector	Emission (dB $\mu$ V)	Limit (dB $\mu$ V)	Margins (dB)
0.270	Neutral	AV	40.51	51.11	-10.60
0.464	Neutral	AV	28.51	46.93	-18.42

**Table 14. Conducted EMI measurement 230 V**

Frequency (MHz)	Phase	Detector	Emission (dB $\mu$ V)	Limit (dB $\mu$ V)	Margins (dB)
0.198	Line	AV	51.59	53.69	-2.10
0.202	Neutral	QP	50.25	63.52	-13.27
0.262	Line	AV	41.29	51.36	-10.07
0.374	Neutral	QP	48.19	58.40	-10.21
0.374	Neutral	AV	35.77	48.41	-12.64
0.398	Neutral	AV	36.59	47.89	-11.30
0.462	Neutral	AV	39.25	46.65	-7.40
0.526	Neutral	AV	37.59	46.00	-8.40
0.570	Line	AV	28.46	46.00	-17.53
0.742	Line	QP	47.43	46.00	-8.56
0.742	Line	AV	30.71	46.00	-15.28
0.766	Line	QP	45.60	46.00	-10.39
0.766	Line	AV	29.19	46.00	-16.80
0.854	Neutral	AV	35.46	46.00	-10.53
1.114	Neutral	AV	33.06	46.00	-12.93
1.186	Neutral	AV	34.50	46.00	-11.49

## 4.2 Immunity against lighting surges

### Test conditions:

- Combination wave: 1.2/50  $\mu$ s open circuit voltage and 8/20  $\mu$ s short-circuit current
- Test voltage: 2 kV
- L1 to L2: 2  $\Omega$ ; L1 to PE, L2 to PE and L1 + L2 to PE: 12  $\Omega$
- Phase angle: 0 °, 90 °, 180 ° and 270 °
- Number of tests: 5 positive and 5 negative
- Pulse repetition rate: 20 s

### Test result:

- There is no disruption of functionality

## 4.3 Immunity against ESD

### Test conditions:

- ESD air discharge at the ground contact of the output cable

### Pass criteria:

- IEC61000-4-2 air discharge level 3 (8 kV) and level 4 (15 kV)

**Table 15. Immunity against ESD**

Performance of the adapter at an ESD air discharge

ESD performance	No disruption of function	Auto recovery
Demo board according to schematic	±12 kV	±15 kV
Demo board with 6 M x 10 M across Y-cap	±16.5 kV	-

#### 4.4 Mains harmonic reduction (MHR)

**Test conditions:**

- The adapter is set to the maximum continuous load of 6.15 A
- The input voltage is 230 V; 50 Hz

**Pass criteria:**

- Compliance with EN61000-3-2 A14 class D

**Test result:**

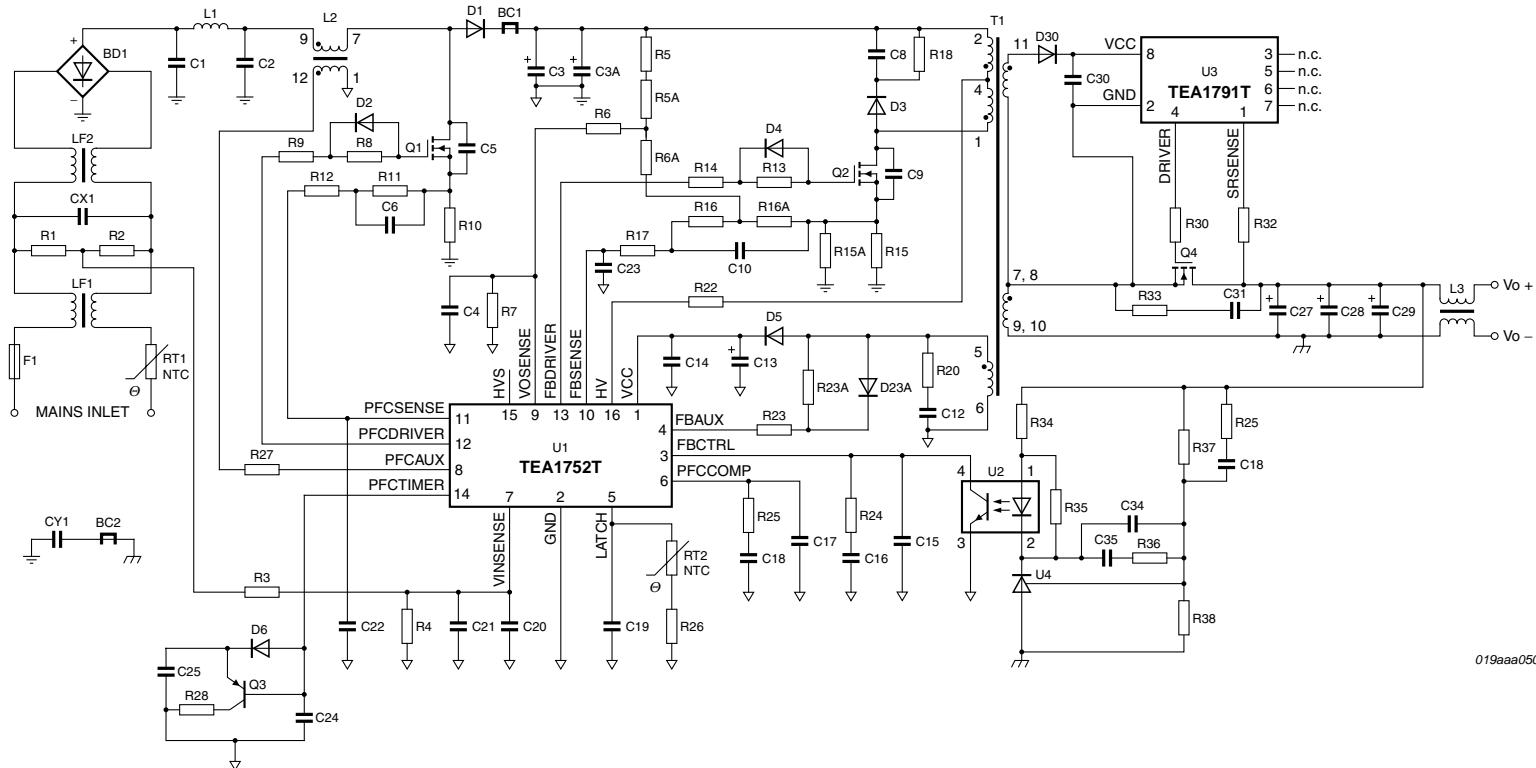
- Passed, see [Table 16](#)

**Table 16. MHR according EN61000-3-2 A14, class D**

Harmonic number	Measured (mA)	Limit (mA)	Harmonic number	Measured (mA)	Limit (mA)
1	588.3	-	21	2.2	26.6
3	110.3	446.9	23	2.6	24.1
5	54.6	249.8	25	7.8	22.0
7	17.5	131.5	27	5.5	20.2
9	10.5	65.7	29	3.7	18.7
11	6.2	46.0	31	5.6	17.5
13	15.0	46.0	33	2.7	16.3
15	8.1	38.9	35	1.5	15.3
17	6.9	33.7	37	3.4	14.5
19	4.4	29.8	39	5.0	13.7

## 5. Schematic

019aaa050



**Fig 14. Schematic of 120 W TEA1752T and TEA1791T adapter solution**

## 6. Bill of materials

**Table 17. Default bill of materials for a 120 W TEA1752T and TEA1791T adapter solution**

Reference	Component	Package	Remark
R1	2 MΩ, 1 %	1206	-
R2	2 MΩ, 1 %	1206	-
R3	560 kΩ, 1 %	1206	-
R4	47 kΩ, 1 %	0603	-
R5	2 MΩ, 1 %	1206	-
R5A	1.3 MΩ, 1 %	1206	-
R6	2.7 MΩ, 1 %	1206	-
R6A	2.7 MΩ, 1 %	1206	-
R7	60.4 kΩ, 1 %	0603	-
R8	10 Ω, 5 %	0805	-
R9	10 Ω, 5 %	0805	-
R10	0.1 Ω, 5 %; 1 W	axial	metal-oxide film
R11	15 kΩ, 5 %	0603	-
R12	1 kΩ, 5 %	0805	-
R13	10 Ω, 5 %	0805	-
R14	10 Ω, 5 %	0805	-
R15	0.1 Ω, 5 %; 1 W	axial	metal-oxide film
R15A	-	-	not mounted
R16	39 kΩ, 5 %	0603	-
R16A	1.2 kΩ, 5 %	0603	-
R17	820 Ω, 5 %	0603	-
R18	43 kΩ, 5 %	1206	-
R19	43 kΩ, 5 %	1206	-
R20	47 Ω, 5 %	0805	-
R21	0 Ω	0805	-
R22	10 kΩ, 5 %	0805	-
R23	82 kΩ, 1 %	0603	-
R23A	330 kΩ, 1 %	0603	-
R24	39 kΩ, 5 %	0603	-
R25	39 kΩ, 5 %	0603	-
R26	10 kΩ, 5 %	0603	-
R27	5.1 kΩ, 5 %	1206	-
R28	0 Ω	0603	-
R29	-	-	not mounted
R30	10 Ω, 5 %	0805	-
R32	1 kΩ, 5 %	0805	-
R33	-	-	not mounted
R34	1 kΩ, 5 %	0603	-

**Table 17. Default bill of materials for a 120 W TEA1752T and TEA1791T adapter solution ...continued**

Reference	Component	Package	Remark
R35	3 kΩ, 5 %	0603	-
R36	10 kΩ, 5 %	0603	-
R37	35.7 kΩ, 1 %	0603	-
R38	5.23 kΩ, 1 %	0603	-
R39	-	-	not mounted
RT1	jumper	-	-
RT2	NTC 100 kΩ; D = 5 mm	radial lead	TTC050104
C1	film capacitor 0.47 µF; 450 V, 10 %	-	-
C2	film capacitor 0.47 µF; 450V, 10 %	-	-
C3	electrolytic capacitor 120 µF; 400V; 105 °C	radial 18 × 32 mm	-
C3A	10 nF; 1 kV; Z5U	Disk 11.5 mm	-
C4	10 nF; 25 V; X7R	0603	-
C5	220 pF; 630 V; NP0	1206	-
C6	0.1 µF; 25 V; X7R	0603	-
C8	3300 pF; 630 V	1206	-
C9	100 pF; 630 V; NP0	1206	-
C10	0.1 µF; 25 V; X7R	0805	-
C12	220 pF; 100 V; NP0	0805	-
C13	electrolytic capacitor 47 µF; 35V; 105 °C	radial 5 × 11 mm	low-impedance type
C14	1 µF; 50 V; Y5V	0805	-
C15	10 nF; 25 V; X7R	0603	-
C16	0.33 µF; 10 V; X7R	0603	timing capacitor; review tolerance
C17	0.33 µF; 10 V; X7R	0603	-
C18	0.47 µF; 10 V; X7R	0603	-
C19	10 nF; 25 V; X7R	0603	-
C20	2.2 µF; 10 V; Y5V	0603	-
C21	2.2 µF; 10 V; Y5V	0603	-
C22	220 pF; 50 V; NP0	0603	10 V is permitted
C23	220 pF; 50 V; NP0	0603	10 V is permitted
C24	1 nF; 50 V; X7R	0603	10 V is permitted
C25	1 µF; 16 V; X7R	0603	10 V is permitted
C27	electrolytic capacitor 680 µF; 25V; 105 °C	Radial 10 × 16 mm	low-impedance type
C28	electrolytic capacitor 680 µF; 25V; 105 °C	Radial 10 × 16 mm	low-impedance type
C29	electrolytic capacitor 680 µF; 25V; 105 °C	Radial 10 × 16 mm	low-impedance type
C30	1 µF; 50 V; Y5V	0805	-
C31	-	-	not mounted
C34	0.1 µF; 25 V; X7R	0603	-
C35	10 nF; 25 V; X7R	0603	-
C36	-	-	not mounted
CX1	0.47 µF; 275 V (AC); X2	MKP	-

**Table 17. Default bill of materials for a 120 W TEA1752T and TEA1791T adapter solution ...continued**

Reference	Component	Package	Remark
CY1	3300 pF; 400 V (AC); Y1	Pitch 10 mm	in the first version of the board a 1000 pF capacitor was used. With this value CISPR22 did not pass.
BD1	GBU806; 8 A; 600 V	Flat/mini	-
D1	MUR460; 4 A; 600 V	DO-201AD	Vishay
D2	1N4148W	SOD-123	-
D3	S2M	SMB	-
D4	1N4148W	SOD-123	-
D5	BAS21	SOT23	NXP Semiconductors, BAS20 is permitted
D6	1N4148	SOD323	-
D23A	BAS21	SOT23	NXP Semiconductors, BAS20 is permitted
D27A	-	-	not mounted
D30	BAS21	SOT23	NXP Semiconductors
Q1	2SK3938	TO220F	-
Q2	2SK3797	TO220F	-
Q3	PMBT4403	SOT23	NXP Semiconductors
Q4	PSMN009-100P	TO220	NXP Semiconductors
U1	TEA1752T	SO16	NXP Semiconductors, GreenChip-III PFC and flyback controller
U2	LTV817B	DIP4-W	CTR 130-260, spacing 10.16 mm
U3	TEA1791T	SO8	NXP Semiconductors, GreenChip-SR controller
U4	D431	SOT-23R	Double Microelectronics
T1	flyback transformer 375 µH	PQ3220	YiLiAN
L1	inductor 220 µH	T60-52	YiLiAN
L2	PFC inductor 250 µH	RM10	YiLiAN
L3	inductor CM 160 µH	T12*6*4	-
LF1	inductor CM 380 µH	T12*6*4	-
LF2	inductor CM 10 MH	T16*12*18	-
BC1	bead core R5B/XP N4/AMAX	RH 4*6*2	placed at cathode of D1
BC2	bead core S6H/JK N6/AMAX	RH 3.5*4.2*1.3	placed at lead of CY1
F1	fuse T 3.15 A; 250 V	LT5	-

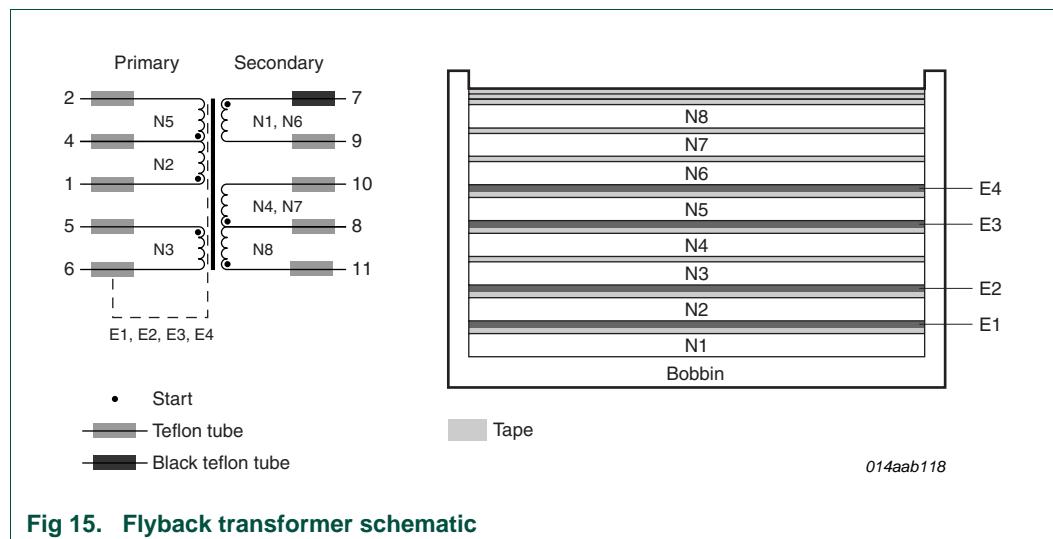
## 7. Transformer and inductor specifications

### 7.1 Flyback transformer T1 specifications

- Primary inductance: 375 µH ( $\pm 5\%$ )
- Leakage inductance: 5 µH (max)
- Core/bobbin: PQ3220
- Core material: PC44

- Hi-POT primary and secondary: 3 kV; 5 mA; 3 s

**Manufacturer:** YiLiAN, LTD, Taiwan ROC.



**Fig 15. Flyback transformer schematic**

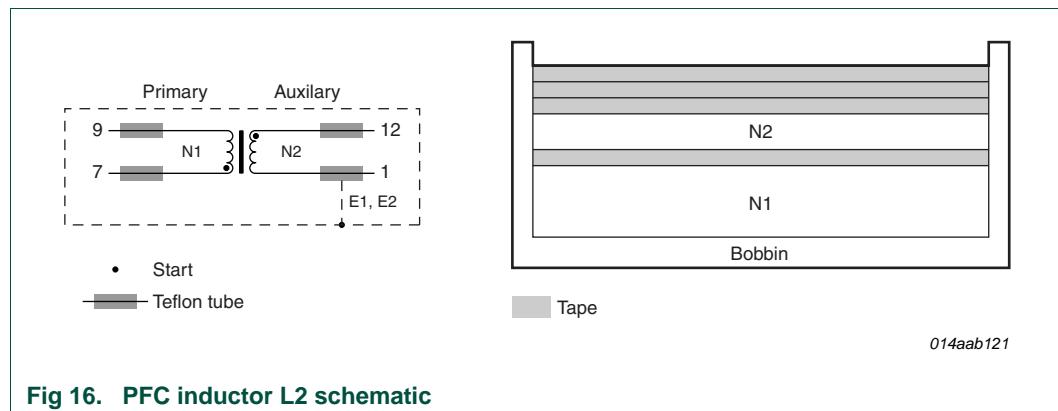
**Table 18. Flyback transformer winding details**

Winding order	Pin number		Wire type	Number of wires	Number of turns		Remarks	
	Start	Finish			Winding	MYLAR tape		
1	N1	7	9	TIW. 0.3 mm diameter	2	6	1	TEX-E
2	E1	-	6	copper foil 0.025 mm × 7 mm	-	1	1	finished with wire 0.3 mm diameter
3	N2	1	4	2UEW 0.5 mm diameter	1	16	1	-
4	E2	-	6	copper foil 0.025 mm × 7 mm	-	1	1	finished with wire 0.3 mm diameter
5	N3	5	6	2UEW 0.25 mm diameter	2	7	1	-
6	N4	8	10	TIW. 0.3 mm diameter	2	6	1	TEX-E
7	E3	-	6	copper foil 0.025 mm × 7 mm	-	1	1	finished with wire 0.3 mm diameter
8	N5	4	2	2UEW 0.5 mm	1	16	1	-
9	E4	-	6	copper foil 0.025 mm × 7 mm	-	1	1	finished with wire 0.3 mm diameter
10	N6	7	9	TIW. 0.3 mm diameter	2	6	1	TEX-E
11	N7	8	10	TIW. 0.3 mm diameter	2	6	1	TEX-E
12	N8	11	8	TIW. 0.3 mm diameter	1	5	3	TEX-E; close winding method

## 7.2 PFC inductor L2 specifications

- Primary inductance: 250  $\mu$ H ( $\pm 10\%$ )
- Core/bobbin: RM10
- Core material: NC-2H

**Manufacturer:** YiLiAN, LTD, Taiwan ROC.



**Table 19. PFC inductor L2 winding details**

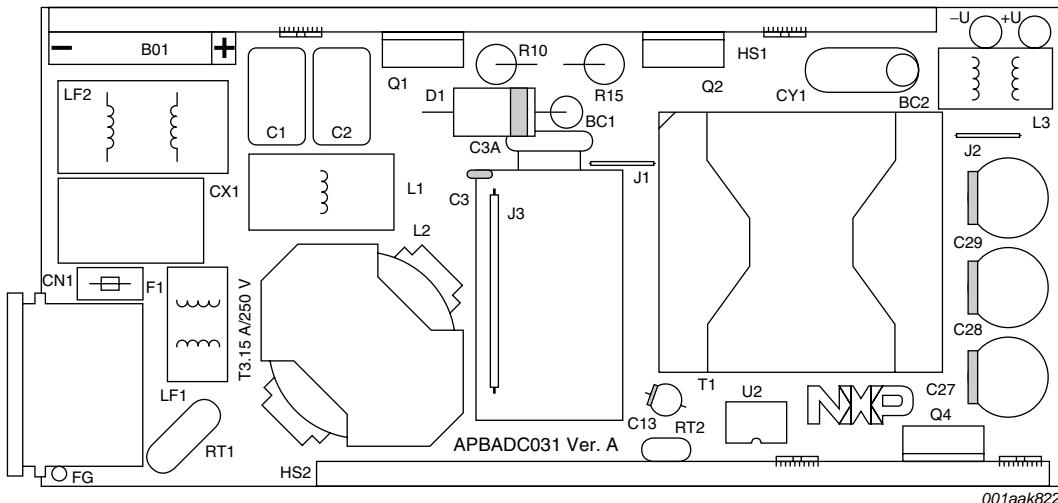
Winding order	Pin no.		Winding type	Number of wires	Number turns		Remarks
	Start	Finish			Winding	MYLAR tape	
1	N1	9	7	USTC 0.1 mm diameter	30	40 turns	1 turn -
2	N2	12	1	2UEW 0.22 mm diameter	2	2.5 turns	3 turns -

## 8. PCB layout

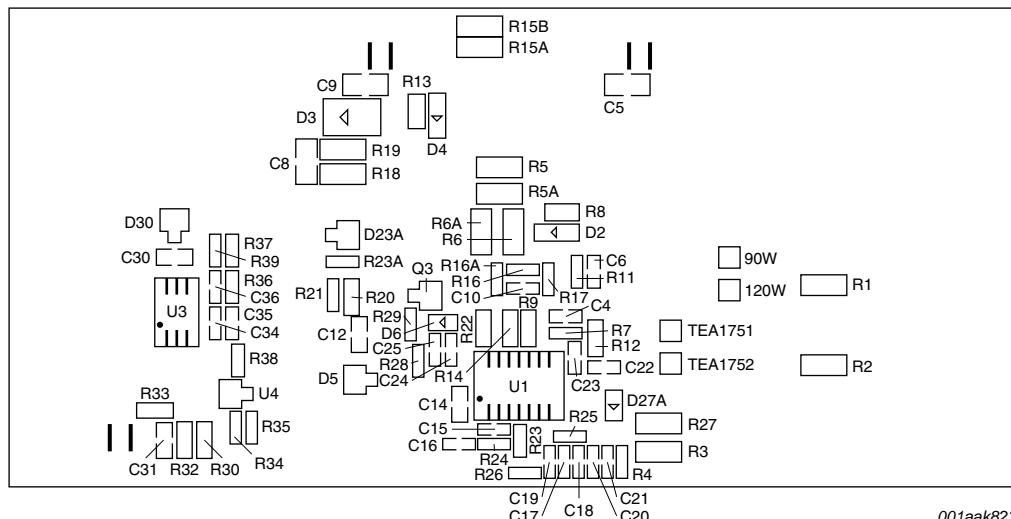
The SMPS printed-circuit board is a single-sided board. Dimensions are 125 mm x 59 mm.

The PCBs are 1.6 mm FR2 with single-sided 2 oz. copper (70 m) layer.

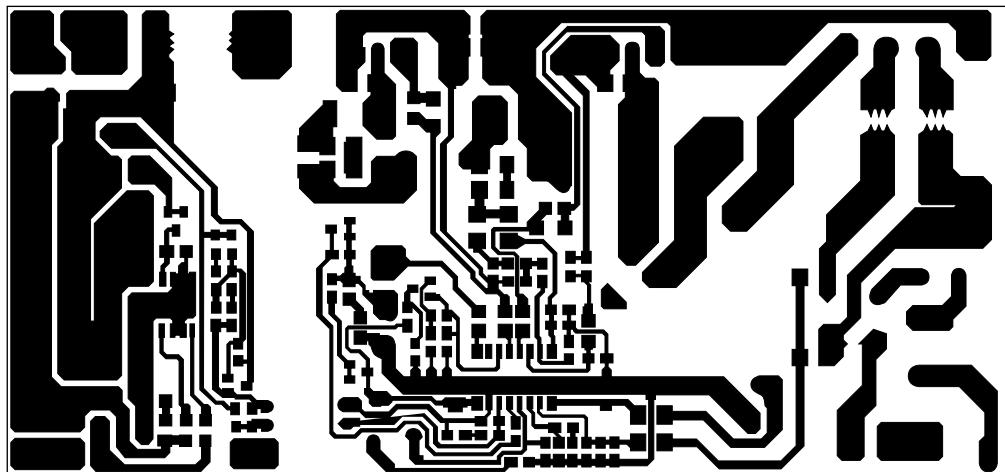
The Gerber file set for production of the PCB is available through the local NXP Semiconductors sales office



**Fig 17. Demo board top silk (top view)**



**Fig 18. Demo board bottom silk (bottom view)**



001aak824

Fig 19. Demo board bottom copper (bottom view)

## 9. Abbreviations

Table 20. Abbreviations table

Acronym	Description
CC	Constant Current
EMC	ElectroMagnetic Compatibility
EMI	ElectroMagnetic Interference
ESD	ElectroStatic Discharge
FLR	Fast Latch Reset
LISN	Line Impedance Standardization Network
MHR	Mains Harmonic Reduction
OTP	OverTemperature Protection
OCP	OverCurrent Protection
OVP	OverVoltage Protection
PE	Protective Earth
PFC	Power Factor Correction
SCP	Short-Circuit Protection
SMPS	Switched Mode Power Supply
SR	Synchronous Rectification
TIW	Triple Insulated Wire
UEW	polyUrethane Enameled Wire
USTC	polyUrethane Silk Tetrone Covered

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